# CFD Analysis in Advance of the NASA Juncture Flow Experiment

June 8, 2017

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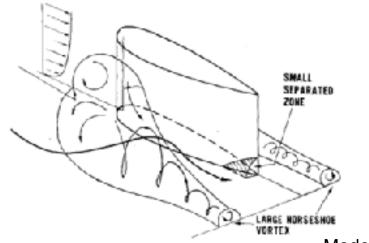
Dan Neuhart
Mike Kegerise
NASA Langley Research Center

#### Juncture Flow

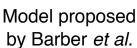


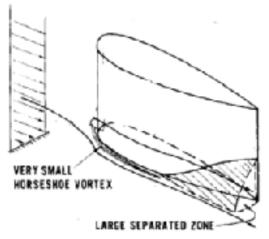
Sponsored by NASA's Transformative Aeronautics Concepts Program's Transformational Tools and Technologies (T³) project

- Substantial effort to investigate the origin of separation bubbles found in wing-body juncture zones
- Primary goal is to gather validation level data, for future CFD code & turbulence model development
- Multi-year effort including several large-scale wind tunnel tests
- Computational Fluid Dynamics (CFD) used in both design and support of risk reduction experiment



(a) thick boundary layer



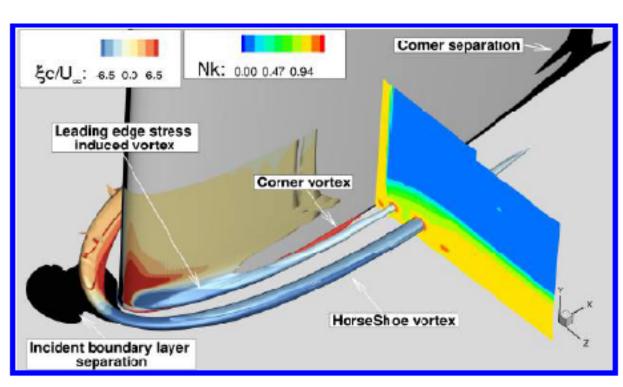


(b) thin boundary layer

#### Background



- Flow physics of juncture flows is complex
  - Several vortical structures coexist: e.g., Horseshoe Vortex (HSV), corner vortex, stress-induced vortex
  - Many factors—such as incoming boundary layer momentum thickness, wing bluntness, and wing sweep—also play some role
- Previous juncture flow work:
  - Simpson et al
  - Gand et al
  - other references mentioned therein



From AIAA-2014-2690 (Bordji et al)

#### Background



- Geometric junctures (corners) are common on aircraft
  - CFD predictive capability is currently uncertain
  - E.g. Drag Prediction Workshops, participants predicted a wide range of wing-body corner separation bubble sizes (none to very large)
- Computed juncture bubble may be influenced by: grid size, grid topology, and numerical treatments
  - Accurate modeling of the Reynolds stresses is needed
  - Non-linear turbulence modeling
- Because of the high degree of uncertainty in the CFD predictions, relevant separated corner flow experiments focused specifically on obtaining high-quality data for CFD validation are needed

#### Past Experiments

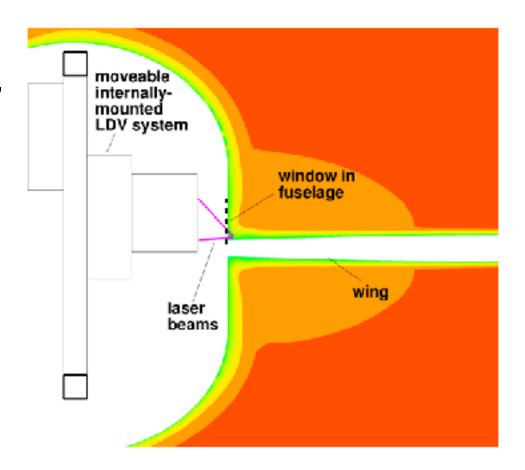


- Simpson et al experiments:
  - Mostly focused on HSV (not so much on corner separation)
- Gand et al experiments:
  - NACA 0012 wing (no sweep) mounted on flat plate did not separate
  - Twisted NACA 0015 wing (no sweep) mounted on flat plate - produced corner separation at alpha=12 deg
- New NASA experiment originally conceived by members of the DPW steering committee
  - Swept wing / fuselage full-span configuration
  - To focus primarily on collecting data for CFD validation
  - A main objective: to obtain flow field details very near the corner

#### Goals and Purpose



- Decision made early: to use internal Laser Doppler Velocimetry (LDV) system
  - Mounted inside of the fuselage on a movable three-axis traverse system
  - Will measure the flow field very near the wing-body juncture through window(s) in the fuselage



#### Goals and Purpose



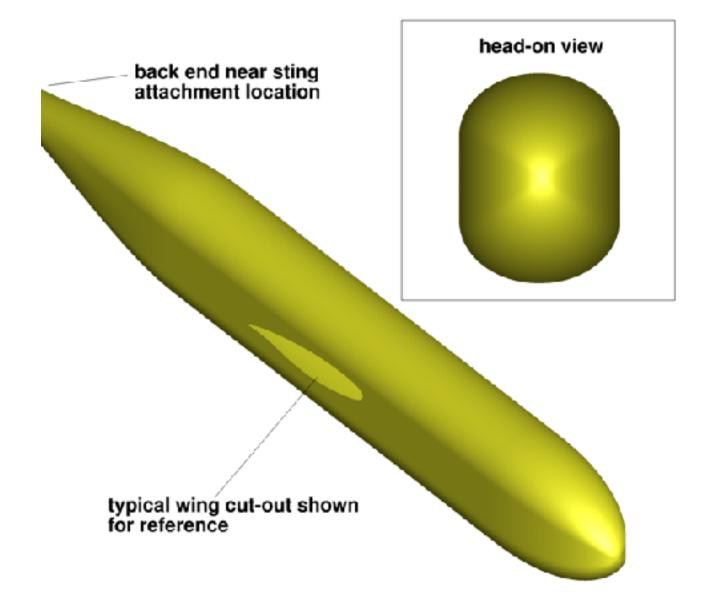
- Decision made to perform a subsonic experiment
  - Subsonic testing venues of sufficient size were readily available
  - M=0.2
  - 8% model based on full scale CRM (~16 ft long, 11 ft wide)
- "CFD Validation-Quality"
  - Boundary conditions, geometry information, experimental uncertainties, etc., necessary for a thorough and unambiguous CFD validation study
  - See, e.g., Aeschliman & Oberkampf (AIAA J 36(5):733-741, 1998)

#### Main purpose:

- Assess the ability of existing models to predict the onset and extent of the three-dimensionally separated flow near the Wing Juncture Trailing Edge region of a full-span wing-body configuration, in terms of the surface topology of the flowfield structure.
- To provide a range of prediction difficulty, a variation of low fields are required, including the onset and progression of corner separation

### Fuselage Configuration

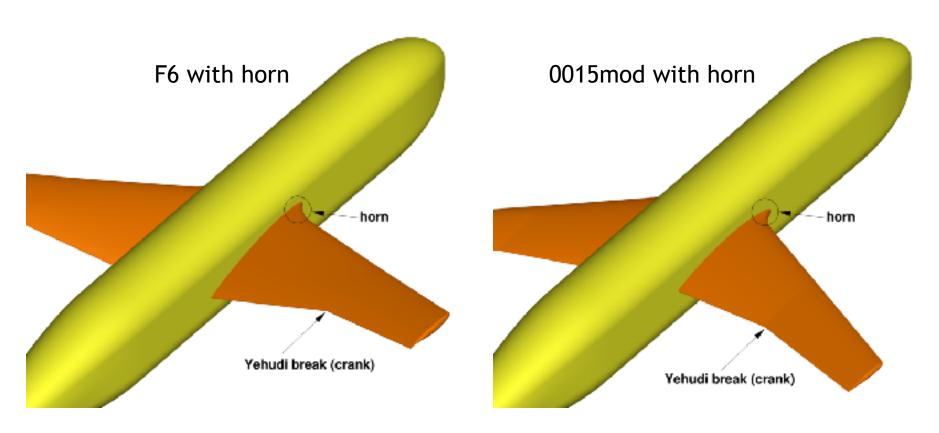




#### Wing Configuration



 Planforms based on truncated DLR-F6 or truncated CRM



### Juncture Flow Model Design



- Preliminary model design done with CFD
  - Overflow 2.2L: SARC-QCR2000
  - Fun3d: SARC-QCR2000
- Evaluated 20+ wing candidates
- Committee down-selected the wing candidates
- Selected 6 wing candidates that combined satisfied the goals
- Risk reduction experiment tests proposed: further evaluate 6 wing candidates

### Wing Candidates

- 6 Wing candidates
- DLR-F6 no horn
  - Used in DPW3
  - Showed side of body separation
- DLR-F6: with LE horn
- NACA 0015 with horn: symmetric wing
- NACA 0015mod: slightly steeper pressure recovery
- F6S12: symmetric F6 variant
- COCA
  - Coder-Campbell design
  - CDISC/skin-friction constraints



COCA

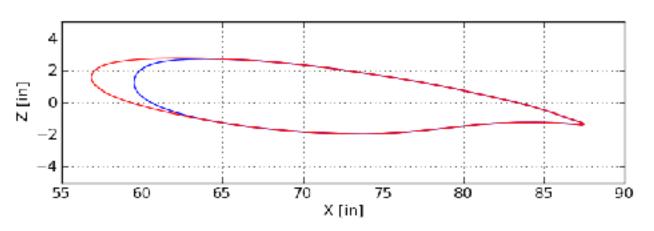
0015

F6-S12

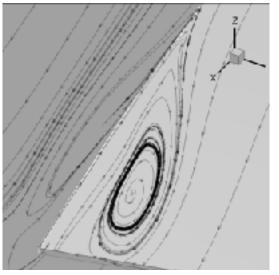
0015mod

#### DLR-F6





Blue: F6 without horn, Red: F6 with horn

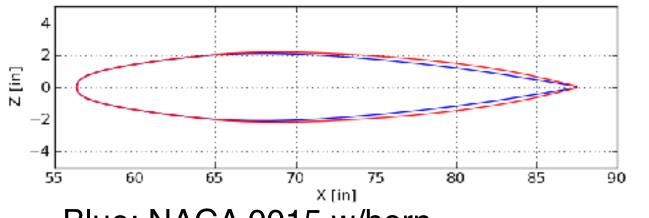


Side of Body Separation

Wing Planform

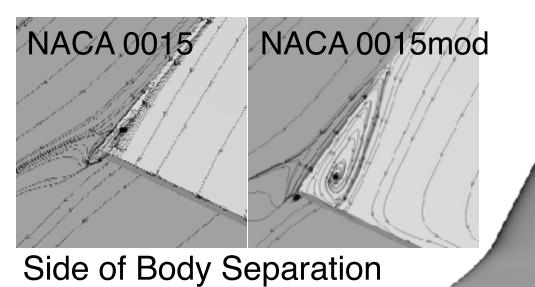
## NACA 0015 — NACA 0015mod





Blue: NACA 0015 w/horn,

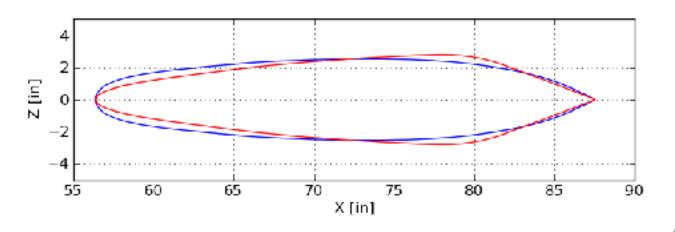
Red: NACA 0015mod with horn



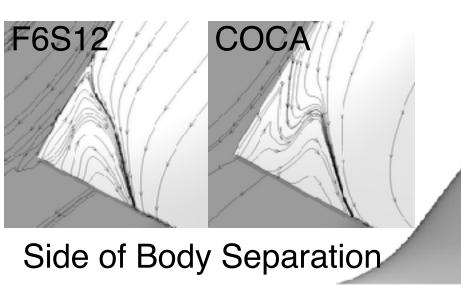
Wing Planform

#### F6S12 — COCA





Blue: F6S12 w/horn, Red: COCA w/horn

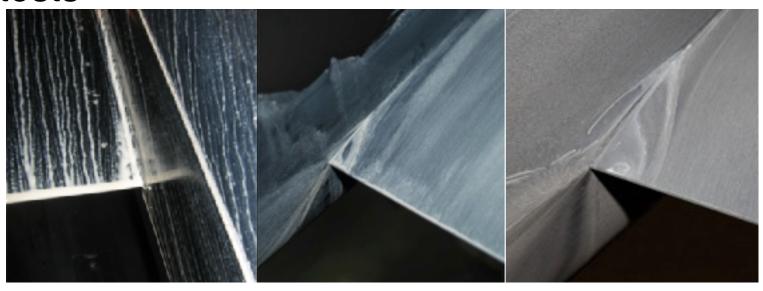


Wing Planform

#### Risk Reduction Tests



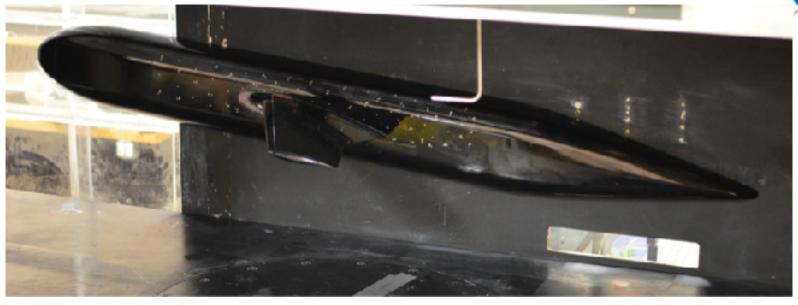
- Series of risk reduction tests
  - Ames TC2 3% wall mounted model, low RE
  - Virginia Tech 2.5% fullspan low RE
  - Langley 14x22 6% fullspan high RE
- CFD solutions were run concurrently with all tests

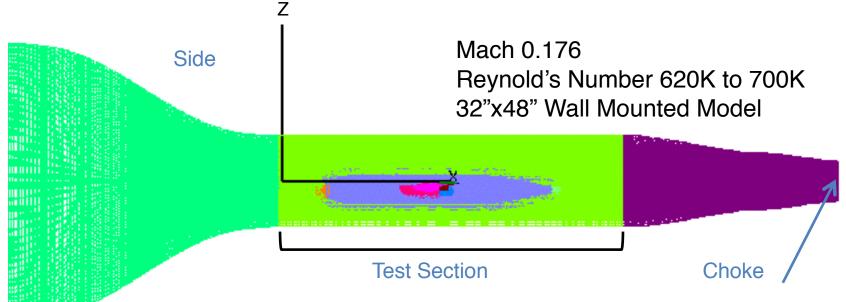


TC2 VA Tech 14x22

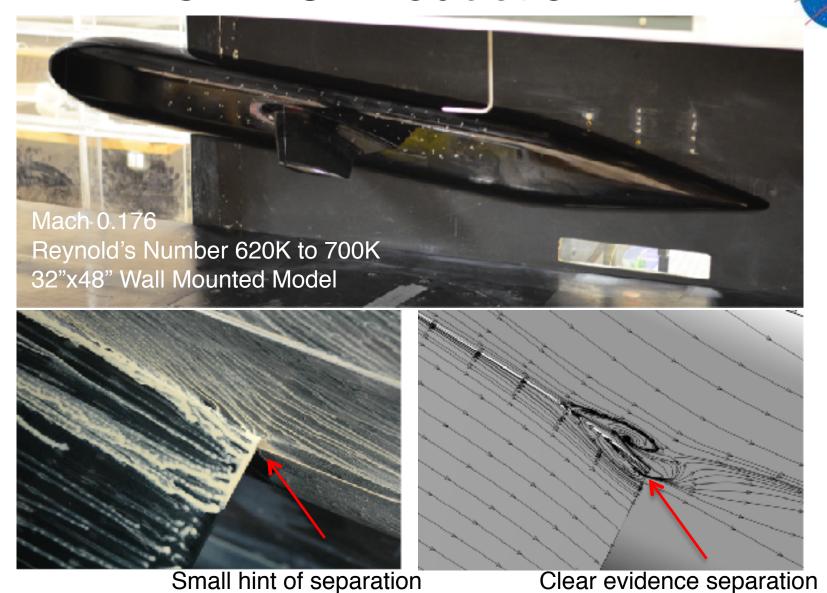
## Model in TC2 and CFD Geometry







#### TC2 Risk Reduction



**Determined Wall Mounted model is not ideal for this test** 

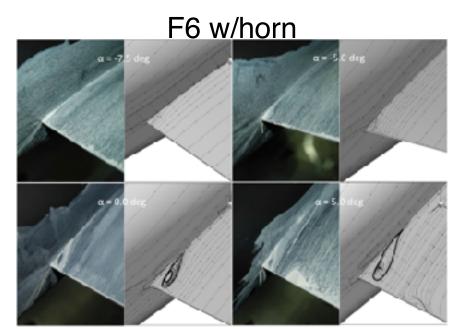
# Virginia Tech 2.5% Full Span Test





Mach 0.176, Reynolds Number of 620K, 6' Test Section



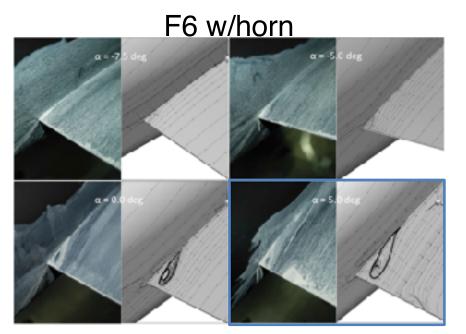


F6S12 w/horn

a = 5.0 deg a = 7.5 deg a = 5.0 deg a = 7.5 deg

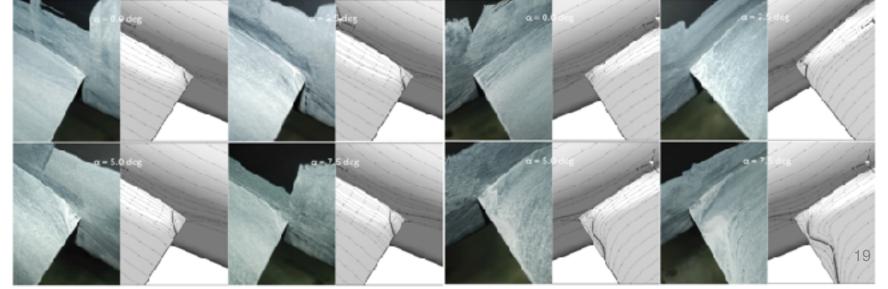
COCA w/horn



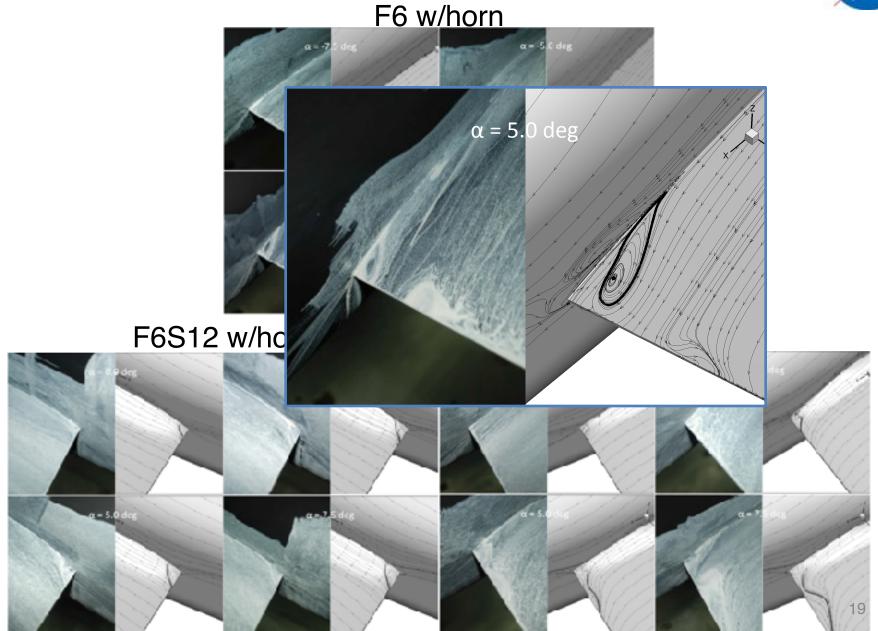


F6S12 w/horn

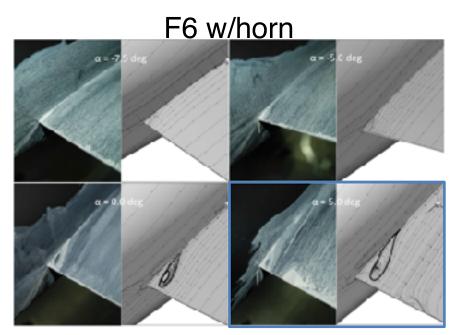
COCA w/horn





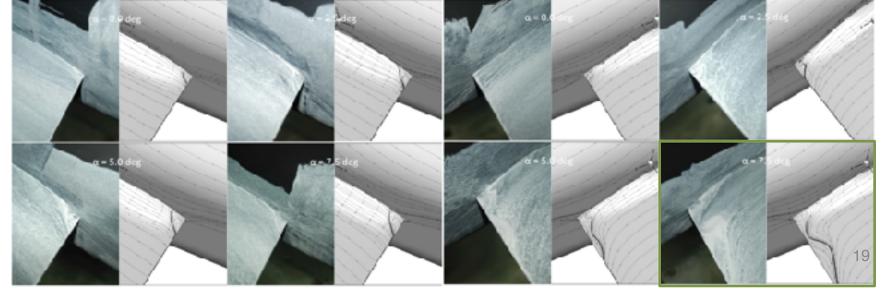




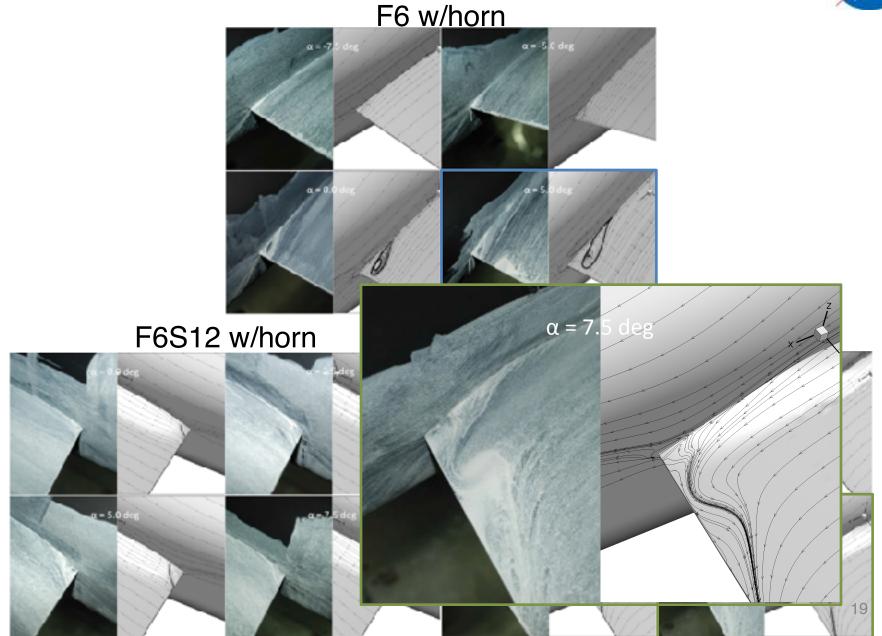


F6S12 w/horn

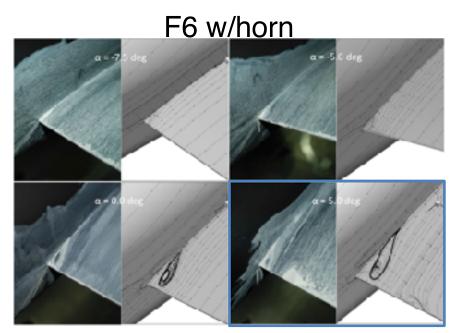
COCA w/horn





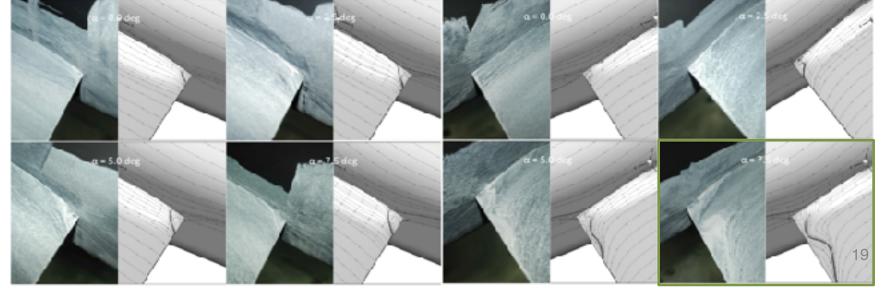






F6S12 w/horn

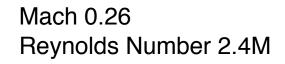
COCA w/horn



### 14x22 6% Risk Reduction Test







## 14x22 6% Risk Reduction Setup

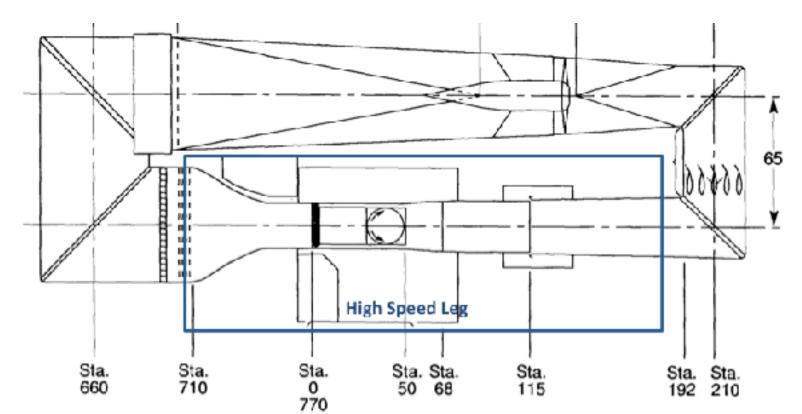


- Three data sources
  - Experiment
  - CFD in Free Air
  - CFD with 14x22 wind tunnel walls
- Comparisons: oil flow vs streamlines
- Additional results for  $\alpha = -10.0 10.0$  degrees in paper
- Additional experimental results in NASA TM-219348

#### NASA Langley 14- by 22-Foot Subsonic Tunnel



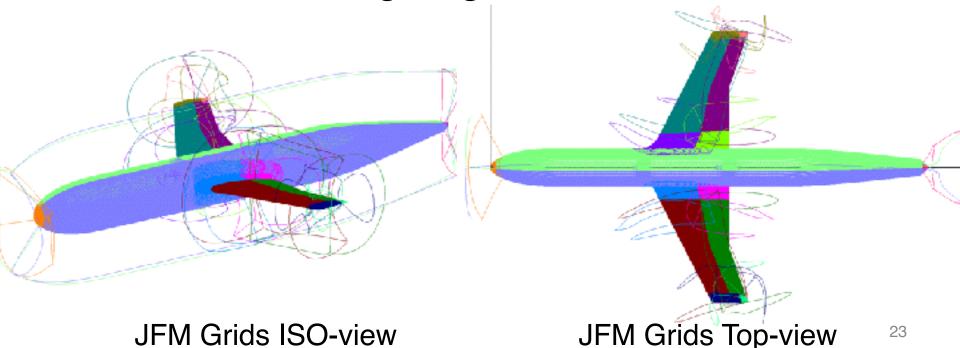
- 14.5 ft high by 21.75 ft wide test section
- Closed-circuit wind tunnel
- Blue box represents high speed leg
- RE = 2.4 million, Mach 0.26



#### Juncture Flow Model Grids



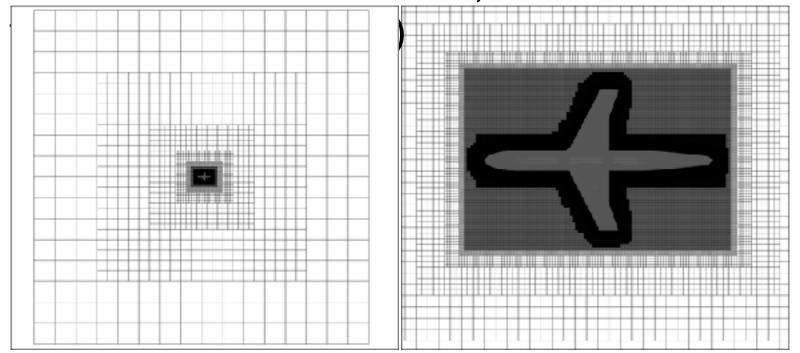
- Grids created based on best practices, as defined by AIAA workshops (DPW, HiLift, etc)
- Grid resolution study was performed early on to establish grid guidelines for all cases



#### JFM Free Air Cases



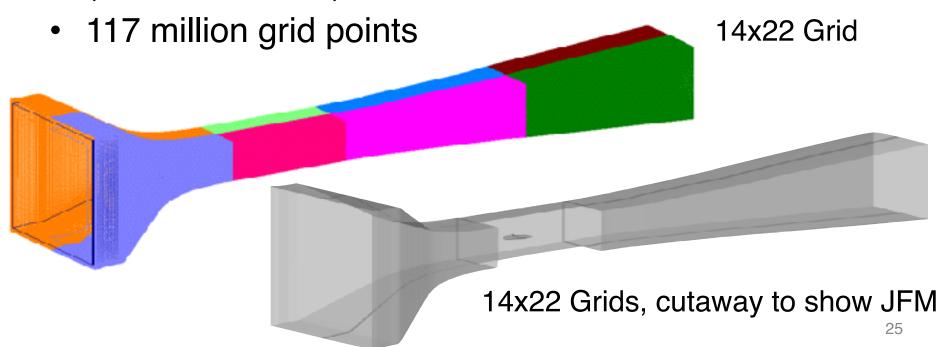
- JFM grids, imbedded in Overflow's off body grids
- Fairfield at 100 chord lengths away
- 108 Million grid points
- 420 Intel Broadwell cores, 12 hours wall



#### JFM Wind Tunnel Cases



- JFM grids, installed in the 14x22 wind tunnel grids
- Inflow BC: Stagnation pressure/temperature
- Outflow BC: Back pressure iterated to match tunnel speed.
- 1200 Intel Ivy Bridge cores, 60-120 hours wall time (NASA Pleiades)

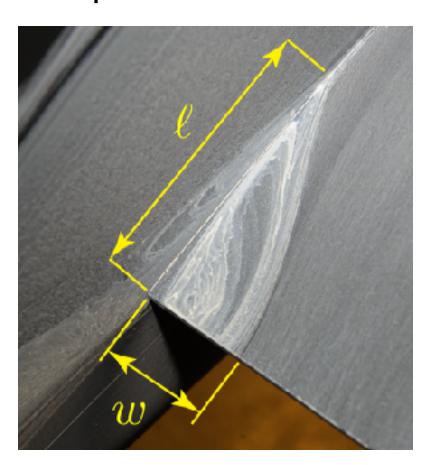


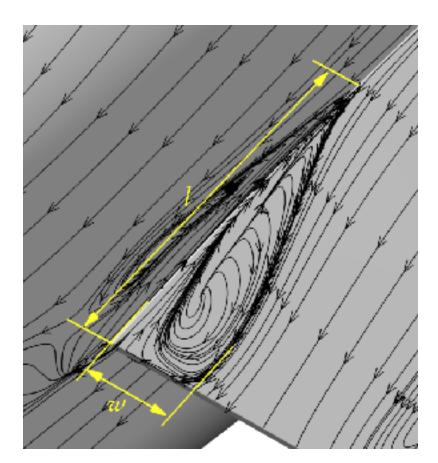
#### SOB Bubble Size Definitions



#### Experiment Oil Flow





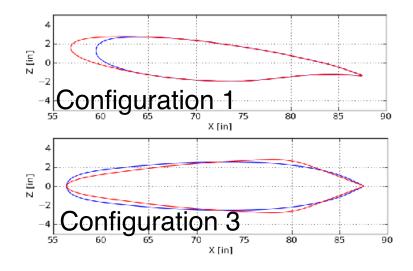


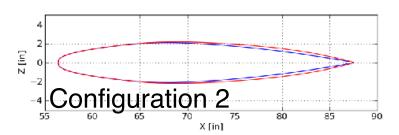
length I and width w bubble size definitions

## Wing Configurations



Configuration	Port Wing	Starboard Wing	Data
1	F6 no horn	F6 w/horn	Exp, CFD Free Air, CFD WT
2	NACA 0015 w/horn	NACA 0015mod w/horn	Exp, CFD Free Air, CFD WT
3	F6S12 w/horn	COCA w/horn	Exp, CFD Free Air



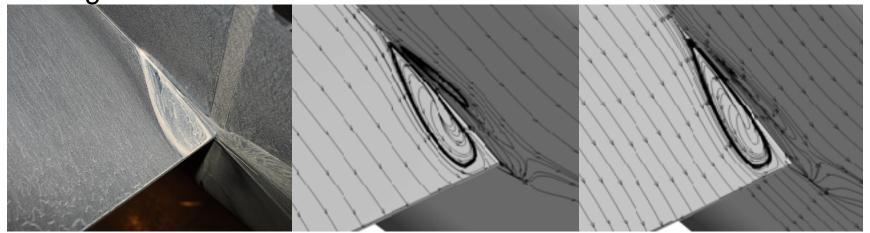


- Port Wing (blue)
- Starboard Wing (red)

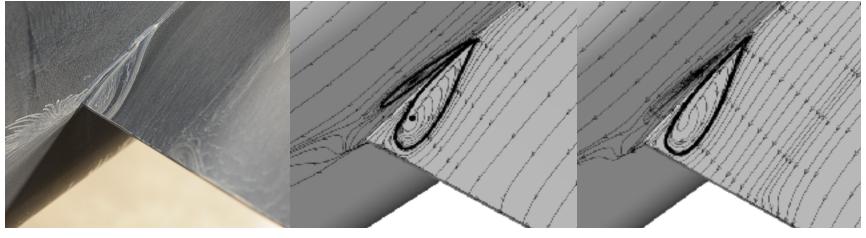
#### Configuration 1: F6 no horn—F6 w/horn, $\alpha = 5.0^{\circ}$



Port Wing: F6 no horn



Starboard Wing: F6 w/horn

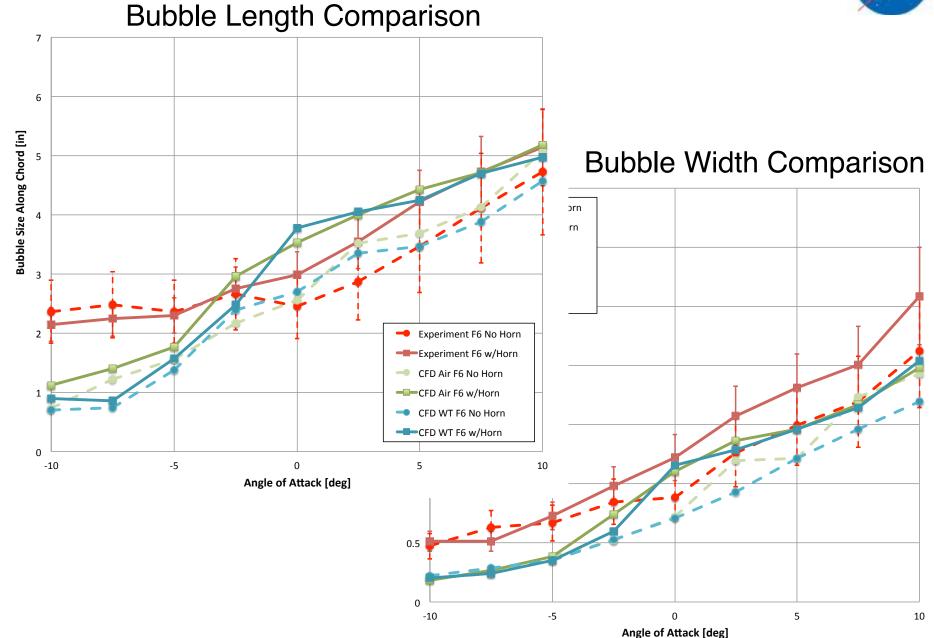


Experiment CFD Free Air

**CFD WT** 

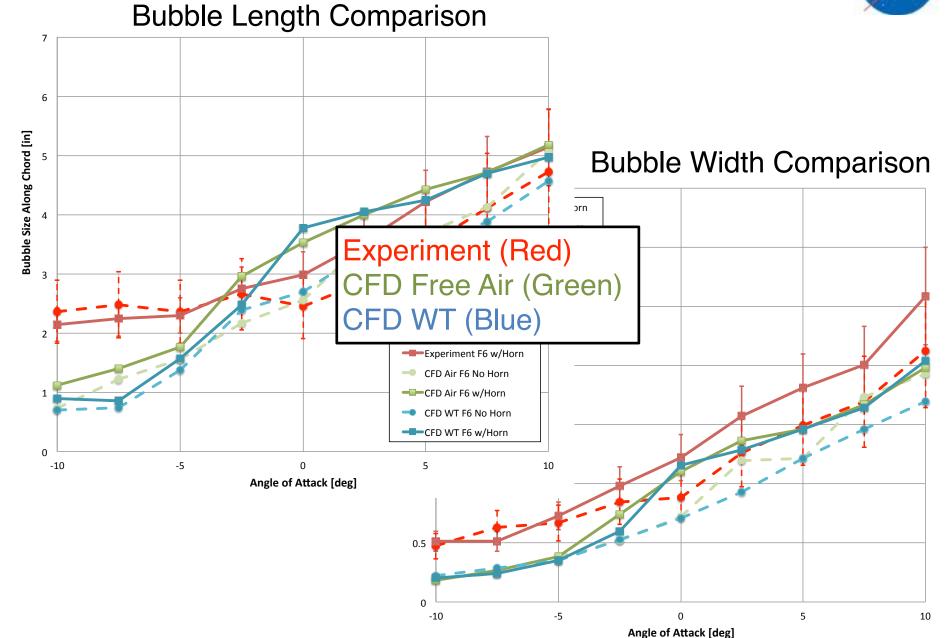
## Configuration 1: F6 no horn—F6 w/horn





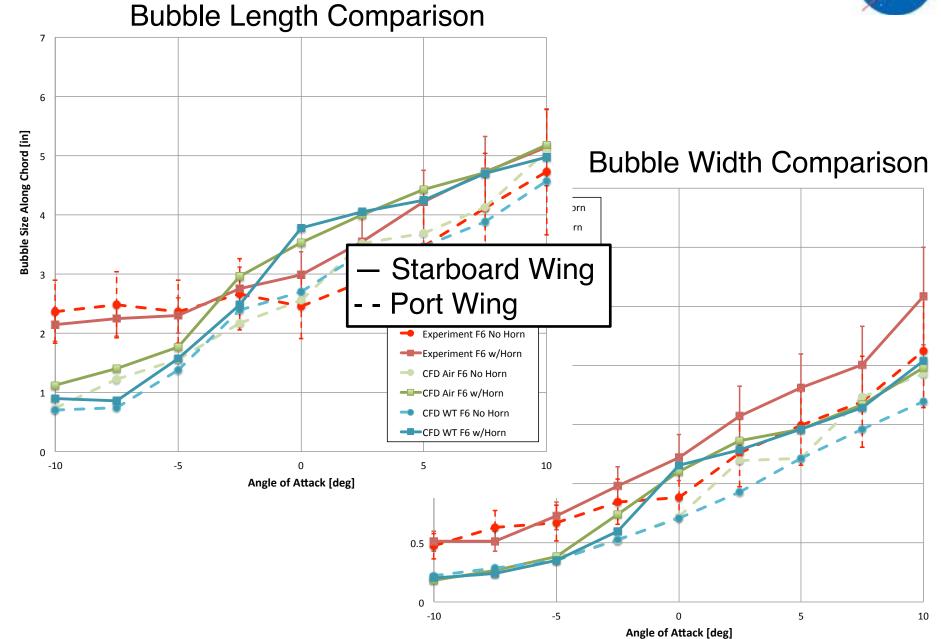
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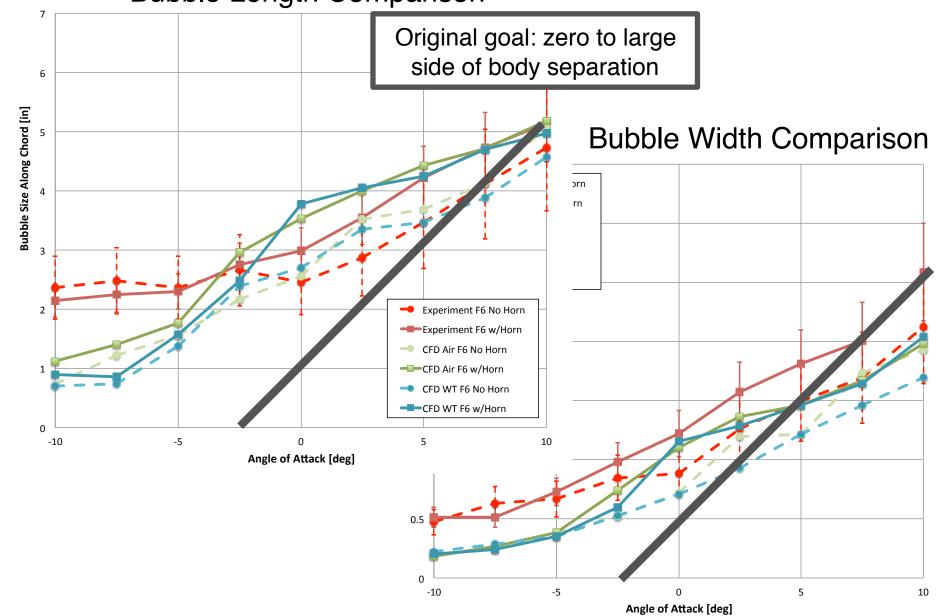




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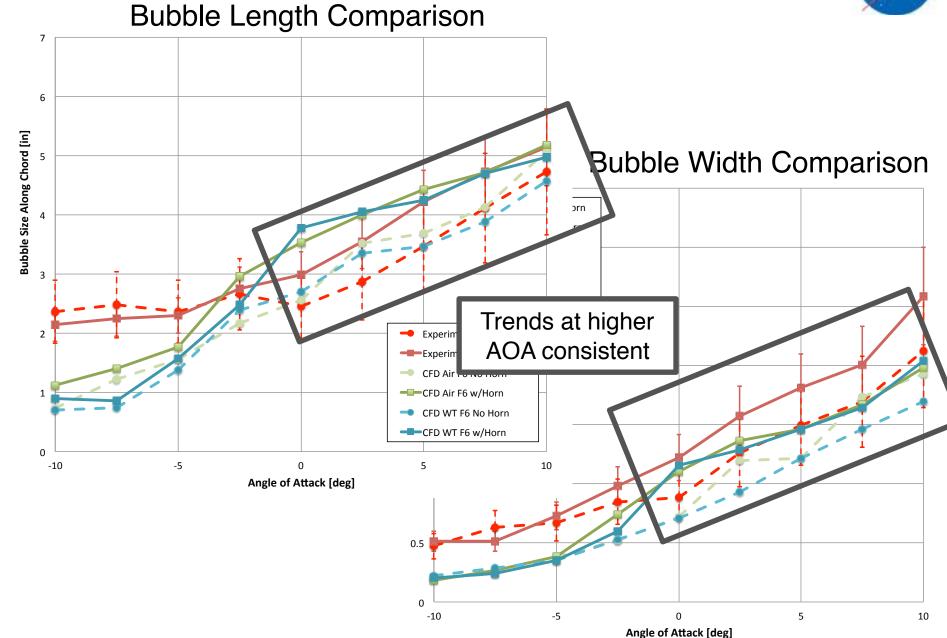


**Bubble Length Comparison** 



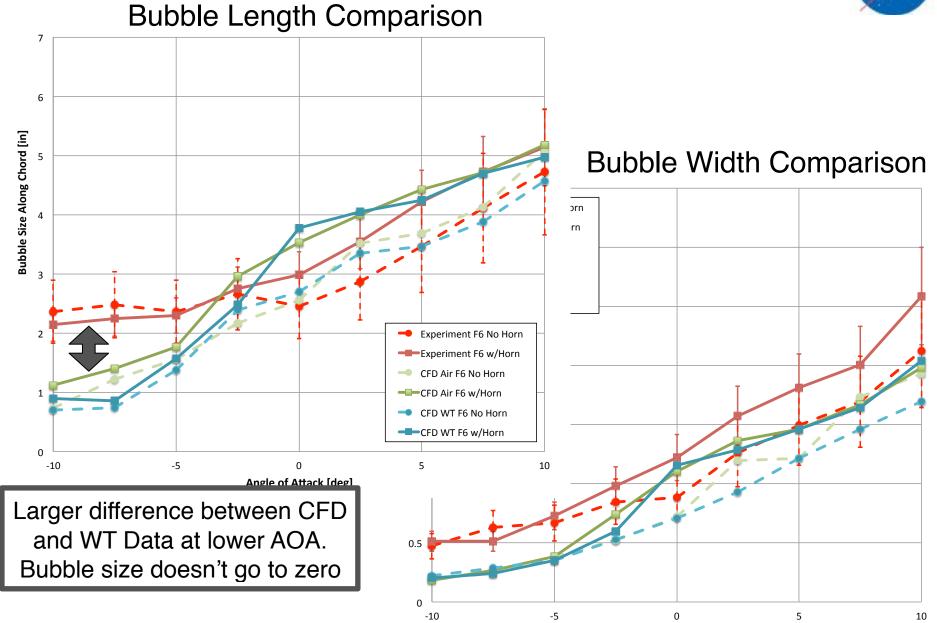
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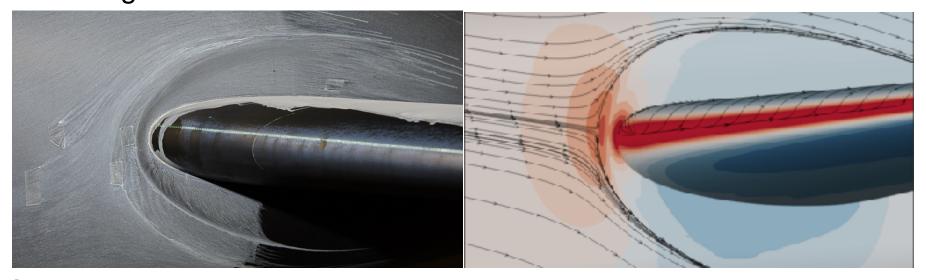
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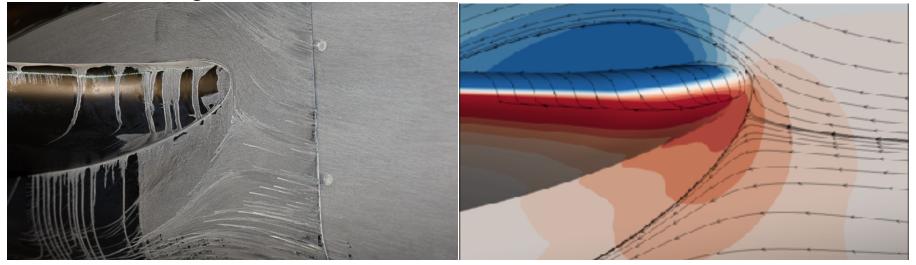


Angle of Attack [deg]

Configuration 1: F6 no horn—F6 w/horn,  $\alpha$ =5.0° LE Port Wing: F6 no horn



Starboard Wing: F6 w/horn



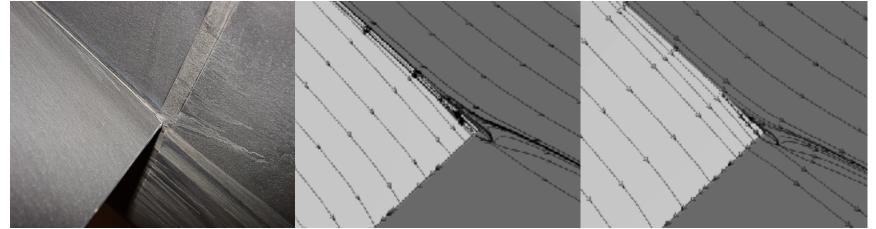
**Experiment** 

**CFD WT** 

#### Configuration 2: NACA 0015—NACA 0015mod, $\alpha$ =5.0°

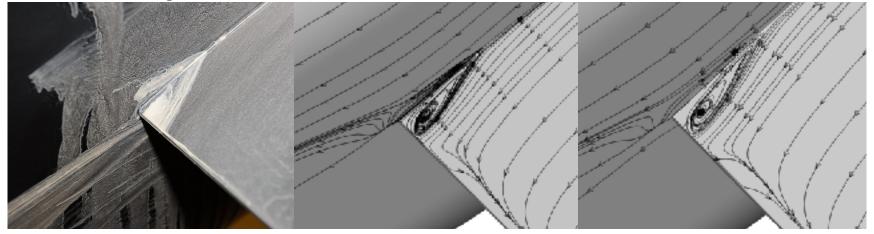


Port Wing: NACA 0015 w/horn



\*Was run without horn

Starboard Wing: NACA 0015mod w/horn



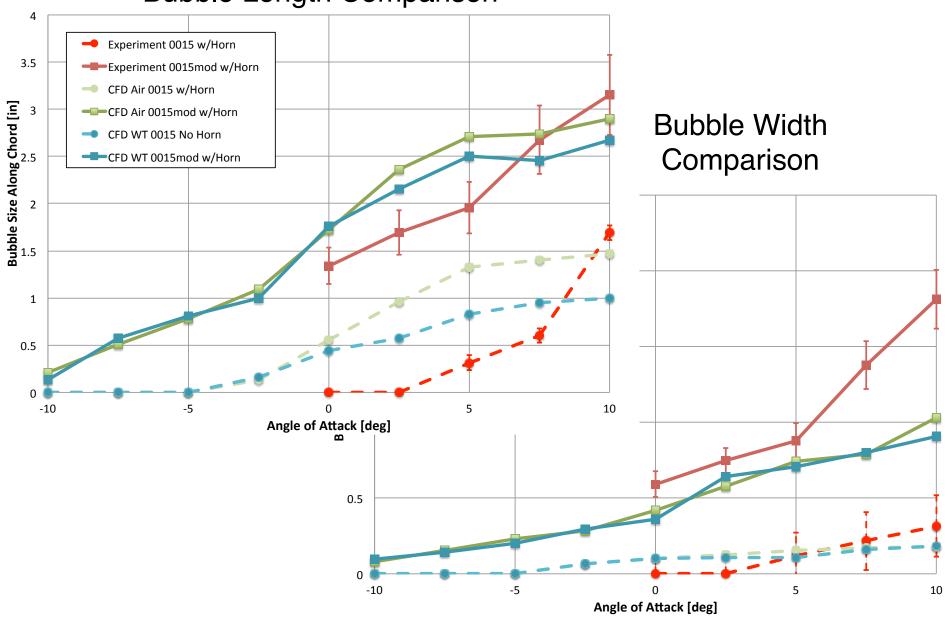
**Experiment** 

CFD Free Air

**CFD WT** 

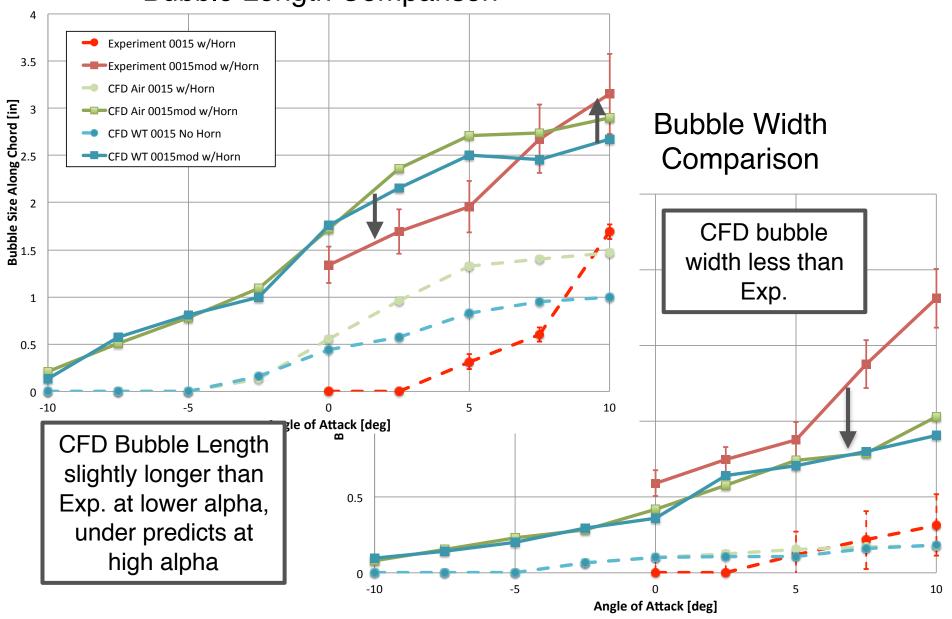






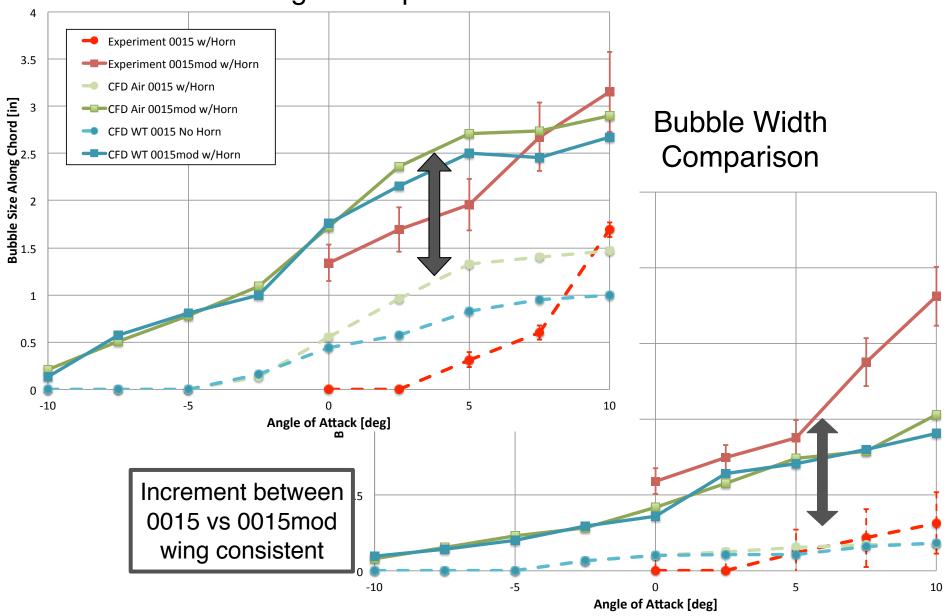






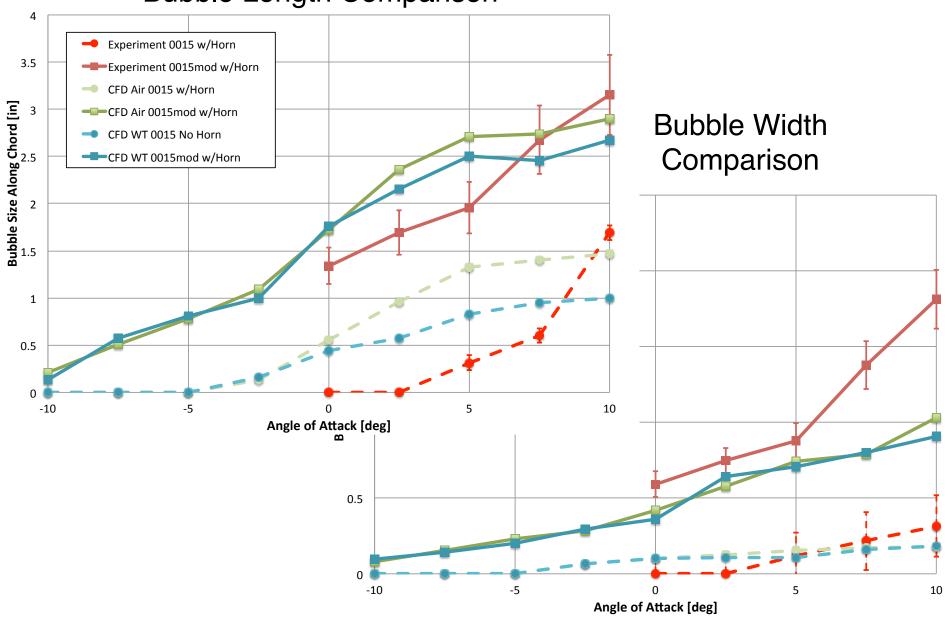






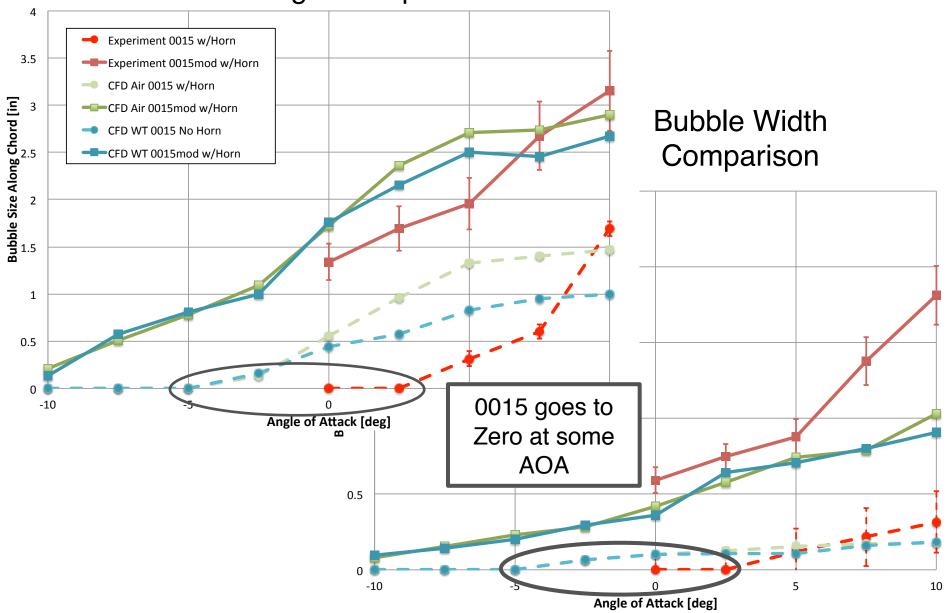












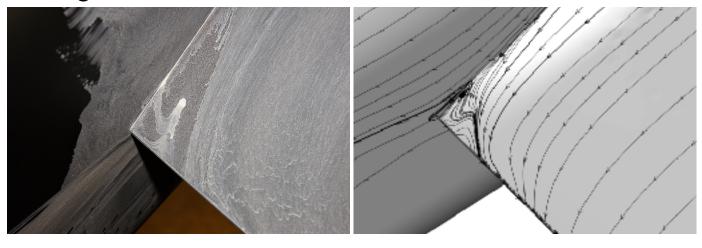
#### Configuration 3: F6S12—COCA, $\alpha$ =5.0°



Port Wing: F6S12 w/horn



Starboard Wing: COCA w/horn



**Experiment** 

**CFD Free Air** 

## Wing Evaluations



- Trends between CFD and Experiment are very good
- F6 showed medium to large side of body separations
- NACA 0015 showed none to small separation
- NACA 0015mod showed small to medium separation
- COCA wing and F6S12 ruled out
- LE-horn indicates smaller LE horseshoe vortex





- Performed wing design evaluations with CFD
- Performed companion CFD risk assessments with the risk reduction experiments
- CFD analysis combined with risk reduction experiments, results in high confidence in selecting the final models



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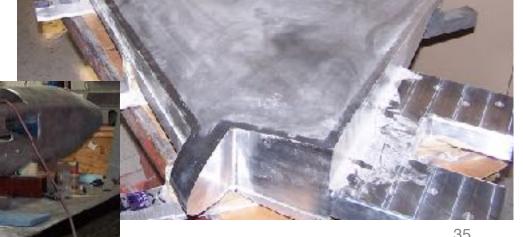


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 Fuselage Model & Wing models delivered May 2017





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 Fuselage Model & Wing models delivered May 2017

Tunnel entry 1: November 2017





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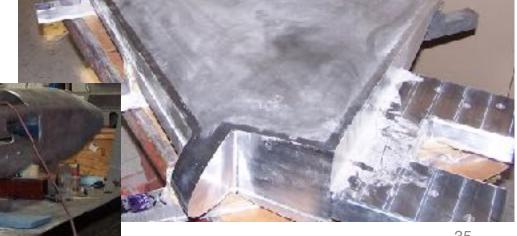
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 Fuselage Model & Wing models delivered May 2017

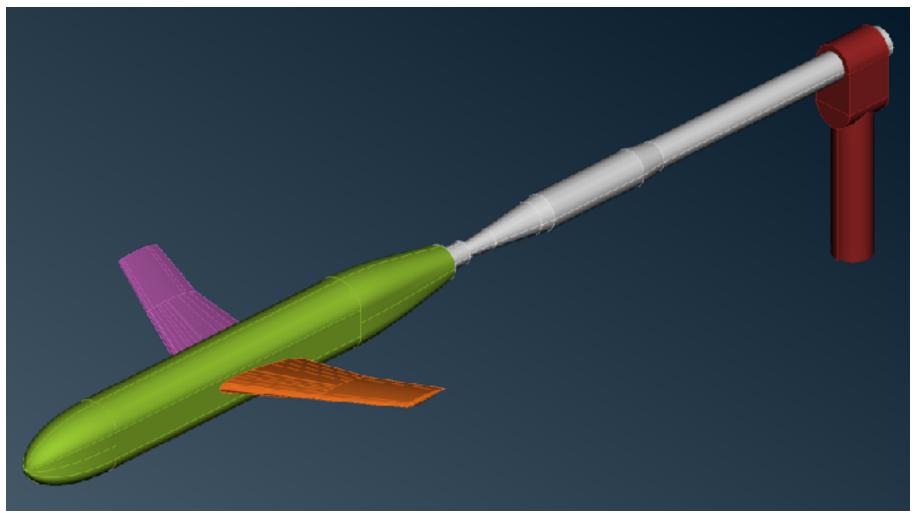
Tunnel entry 1: November 2017

Tunnel entry 2: March 2018



# **Upcoming CFD**



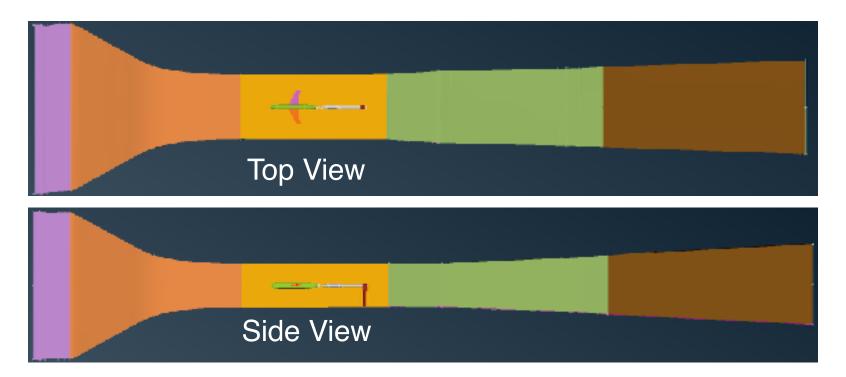


Mock up of the JFM 8% model with roll sting and mast

#### **Upcoming CFD**



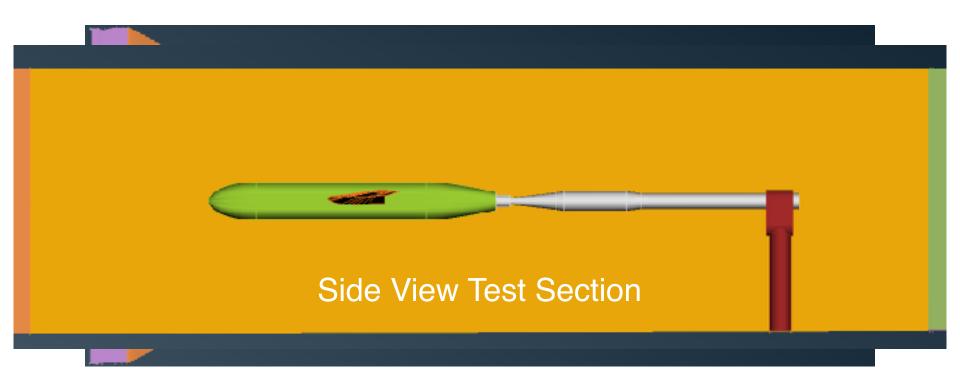
- Run with Overflow & Fun3D
- Incremental buildup
  - Free air: JFM, JFM + Sting, JFM + Sting + Mast
  - 14x22 WT: JFM, JFM + Sting, JFM + Sting + Mast



## **Upcoming CFD**



- Run with Overflow & Fun3D
- Incremental buildup
  - Free air: JFM, JFM + Sting, JFM + Sting + Mast
  - 14x22 WT: JFM, JFM + Sting, JFM + Sting + Mast



## Acknowledgements



NASA's Transformational Tools and Technologies (T3) Project

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Virginia Tech: Aurelien Borgoltz and Todd Lowe

University of Kentucky: Jim Coder

Bill Oberkampf